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Patentanmeldung Nr. Patent application No. Demande de brevet n°

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**Blatt 2 der Bescheinigung
Sheet 2 of the certificate
Page 2 de l'attestation**

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Optical scanning head.

24. 12. 1999

(90)

The invention relates to an optical head for scanning an optical record carrier

having an information layer, the head comprising a radiation source for generating a radiation beam, an optical system for converging the radiation beam to a focus on the information layer, the optical system imparting a temperature-dependent first wavefront deviation to the radiation beam, and a compensator arranged in the radiation beam for compensating the first wavefront deviation. The invention also relates to a set of optical elements comprising an optical element and a compensator, the optical element being arranged in the path of a radiation beam and imparting a temperature-dependent first wavefront deviation to the radiation beam, the compensator being arranged in the path of the radiation beam for compensating the first wavefront deviation.

The increase in the information density of record carriers in the field of optical recording is accompanied by a commensurate decrease of the size of the radiation spot for scanning the record carrier. The decrease of the spot size is achieved by shorter wavelengths and higher numerical apertures (NA) of the radiation beam incident on the record carrier.

These factors narrow the tolerances of the optical components in an optical scanning head. In particular, the effect of environmental influences on the components becomes noticeable. Temperature changes affect the refractive index and shape of a lens, causing, amongst others, a change of the focal distance, also called defocus, and the introduction of spherical aberration. In general, an optical head comprises a collimator lens and an objective lens. The most important temperature-induced wavefront deviation for the objective lens is spherical aberration; defocus is less important because any change in the position of the focal spot will automatically be corrected by an automatic focus servo system. Since the NA of the radiation beam incident on the collimator lens is relatively small, the most important temperature-induced wavefront deviation for the collimator lens is defocus. The fixed position of the collimator lens with respect to the radiation source causes defocus to change the conjugates of the collimator lens away from the design conjugates, resulting in aberrations. The narrower tolerances limit the possibilities to employ plastic for the manufacture of the lenses because most plastics are highly susceptible to changes in temperature. Several proposals have been put forward to reduce the effect of temperature changes.

One solution is to adapt the shape of the lenses in the optical head and to choose lens materials having a specific temperature variation of the refractive index. Such an optical head is known from the US patent no. 4,753,524. A drawback of this optical head is, that the design freedom is strongly reduced by the requirements imposed on the lens shapes and the choice of materials. It might even necessitate the use of a third lens in the optical head.

Another solution is disclosed in European patent application no. 0 632 905, in which a diffractive structure is arranged in the optical path. The structure has a temperature-dependent grating period, causing the direction of the diffracted beam to depend on the temperature. An appropriate combination of the diffractive structure and one or more lenses can reduce the effects of temperature changes. Although a grating can be designed to yield 100% efficiency, actual gratings never attain such a high efficiency. This reduction of the efficiency of the light path of the optical head is disadvantageous in optical recorders, which require a large amount of radiation energy for writing information in the record carrier.

It is an object of the invention to provide an optical head in which the effects of temperature changes have been reduced without the above mentioned disadvantages.

This object is achieved if, according to the invention, the compensator comprises a phase structure of a material having temperature-dependent properties, the phase structure having the form of annular areas forming a non-periodic pattern of optical paths of different, temperature-dependent lengths, the optical paths forming a second wavefront deviation compensating the temperature-dependent first wavefront deviation. If the material of the phase structure and the optical paths of the annular areas are properly chosen, the phase structure of the annular areas introduce a wavefront deviation in the radiation beam having the correct shape and temperature dependence to compensate the wavefront deviation of the optical system. The phase structure does not impose restrictions on the elements of the optical system, thereby leaving a great freedom of design.

It should be noted, that the phase structure according to the invention has a non-periodic pattern, and, therefore, does not form diffraction orders. As a consequence, the phase structure does not have the inherent losses of a grating. The compensator is therefore very suitable for use in an optical head that requires a change in wavefront in dependence on the temperature, because the phase structure can introduce the required temperature-dependent wavefront changes without appreciable loss of radiation energy.

In a preferred embodiment the optical head comprises an objective system imparting spherical aberration as the first wavefront deviation to the radiation beam. Since the thermally induced defocus will be corrected for automatically by the focus servo system, the

spherical aberration need only be compensated, which can advantageously be carried out by the compensator.

In another embodiment of the optical head the optical system comprises a collimator lens and an objective lens, the collimator lens being arranged closer to the radiation source than the objective lens, the objective lens imparting defocus as the first wavefront aberration to the radiation beam. Since the collimator is used in a low-NA radiation beam, the temperature-induced spherical aberration is small and does not require compensation. The thermally induced defocus will cause the collimator lens to operate outside its design conjugates, resulting elsewhere in the optical path in aberrations such as spherical aberration. Therefore, the defocus is preferably compensated by the compensator.

A further aspect of the invention relates to a set of optical elements comprising an optical element and a compensator, the optical element being arranged in the path of a radiation beam and imparting a temperature-dependent first wavefront deviation to the radiation beam, the compensator being arranged in the path of the radiation beam for compensating the first wavefront deviation, in which the compensator comprises a phase structure of a material having temperature-dependent properties, the phase structure having the form of annular areas forming a non-periodic pattern of optical paths of different, temperature-dependent lengths, the optical paths forming a second wavefront deviation compensating the temperature-dependent first wavefront deviation. The optical element is preferably an objective system or a collimator lens.

In a preferred embodiment of the optical set the differences between the optical paths at a design temperature are multiples of the first wavelength. The phase structure will not affect the radiation beam at the design temperature, whereas it will introduce a wavefront deviation in the radiation beam at different temperatures.

In a special embodiment of the optical set, the wavefront deviation is spherical aberration. The compensation of the spherical aberration allows the use of plastic as material for the objective lenses.

In a special embodiment of the optical set the wavefront deviation is defocus. Defocus is a wavefront deviation that is quadratic in the radius of the radiation beam. The quadratic form modulo the wavelength can be approximated by the wavefront steps introduced in the radiation beam by the annular areas. The change in focal position caused by the defocus can advantageously be used in an optical head of a recorder by compensating the thermally induced defocus of the collimator lens.

The objects, advantages and features of the invention will be apparent from the following more particular description of preferred embodiments of the invention, as illustrated in the accompanying drawings, in which

Figure 1 shows a scanning device according to the invention;

5 Figure 2 shows a cross-section of the compensator;

Figure 3 shows the wavefront aberration of the objective lens at an elevated temperature; and

Figure 4 shows the wavefront aberration of the combination of the objective lens and the compensator at the elevated temperature.

10

Figure 1 shows a device 1 for scanning an optical record carrier 2. The record carrier comprises a transparent layer 3, on one side of which an information layer 4 is arranged. The side of the information layer facing away from the transparent layer is protected from environmental influences by a protection layer 5. The side of the transparent layer facing the device is called the entrance face 6. The transparent layer 3 acts as a substrate for the record carrier by providing mechanical support for the information layer. Alternatively, the transparent layer may have the sole function of protecting the information layer, while the mechanical support is provided by a layer on the other side of the information layer, for instance by the protection layer 5 or by a further information layer and a transparent layer connected to the information layer 4. Information may be stored in the information layer 4 of the record carrier in the form of optically detectable marks arranged in substantially parallel, concentric or spiral tracks, not indicated in the Figure. The marks may be in any optically readable form, e.g. in the form of pits, or areas with a reflection coefficient or a direction of magnetization different from their surroundings, or a combination of these forms.

25

The scanning device 1 comprises a radiation source 11 that can emit a radiation beam 12. The radiation source may be a semiconductor laser. A beam splitter 13 reflects the diverging radiation beam 12 towards a collimator lens 14, which converts the diverging beam 12 into a collimated beam 15. The collimated beam 15 is incident on a transparent compensator 16, which modifies the wavefront of the collimated beam in dependence on the temperature in the scanning device. The beam 17 coming from the compensator 16 is incident on an objective system 18. The objective system may comprise one or more lenses and/or a grating. The objective system 18 has an optical axis 19. The objective system 18 changes the beam 17 to a converging beam 20, incident on the entrance face 6 of the record carrier 2. The objective system has a spherical aberration correction adapted for passage of the radiation

30

beam through the thickness of the transparent layer 3. The converging beam 20 forms a spot 21 on the information layer 4. Radiation reflected by the information layer 4 forms a diverging beam 22, transformed into a substantially collimated beam 23 by the objective system 18 and subsequently into a converging beam 24 by the collimator lens 14. The beam splitter 13

5 separates the forward and reflected beams by transmitting at least part of the converging beam 24 towards a detection system 25. The detection system captures the radiation and converts it into electrical output signals 26. A signal processor 27 converts these output signals to various other signals. One of the signals is an information signal 28, the value of which represents information read from the information layer 4. The information signal is processed by an
10 information processing unit for error correction 29. Other signals from the signal processor 27 are the focus error signal and radial error signal 30. The focus error signal represents the axial difference in height between the spot 21 and the information layer 4. The radial error signal represents the distance in the plane of the information layer 4 between the spot 21 and the centre of a track in the information layer to be followed by the spot. The focus error signal and
15 the radial error signal are fed into a servo circuit 31, which converts these signals to servo control signals 32 for controlling a focus actuator and a radial actuator respectively. The actuators are not shown in the Figure. The focus actuator controls the position of the objective system 18 in the focus direction 33, thereby controlling the actual position of the spot 21 such that it coincides substantially with the plane of the information layer 4. The radial actuator
20 controls the position of the objective lens 18 in a radial direction 34, thereby controlling the radial position of the spot 21 such that it coincides substantially with the central line of track to be followed in the information layer 4. The tracks in the Figure run in a direction perpendicular to the plane of the Figure.

The device of Figure 1 may be adapted to scan also a second type of record
25 carrier having a thicker transparent layer than the record carrier 2. The device may use the radiation beam 12 or a radiation beam having a different wavelength for scanning the record carrier of the second type. The NA of this radiation beam may be adapted to the type of record carrier. The spherical aberration compensation of the objective system must be adapted accordingly.

30 The objective system 18 shown in Figure 1 is formed by a single lens having an NA of 0.65 for operation at a wavelength of 650 nm. The lens is made of COC (Topas). At the design temperature T_0 of 20 °C the lens has the correct spherical aberration compensation for the transparent layer 3 of the record carrier 2. When the temperature of the objective lens deviates from T_0 , the change in shape of the lens and in the value of the refractive index causes

additional spherical aberration to be introduced in the radiation beam. Since this aberration is not required for the compensation of the spherical aberration introduced by the transparent layer 3, the aberration will reduce the quality of the focal spot 21. The compensator 16 is adapted to compensate the temperature-dependent spherical aberration of the objective lens.

5 Figure 2 shows a cross-section of the compensator 16. The compensator comprises a transparent plate 50, one surface of which is a phase structure, which is rotationally symmetric around the optical axis 19. The phase structure has a central area 51 and four concentric annular areas 52, 53, 54 and 55. The annular areas 52, 53 and 54 are rings with a height of h_1 , h_2 and h_3 above the height of the central area 51. The height of the areas is exaggerated with respect to the thickness and radial extent of the plate 50. The rings are made of a material having a refractive index $n(T)$, where T is the temperature of the compensator. 10 The plate 50 may also be made of the same material as the rings. The heights h_j are each equal to $m_j h$, with m_j an integer and h equal to

$$h = \frac{\lambda}{n(T_0) - 1} \quad (1)$$

15 where λ is the wavelength and $n(T_0)$ is the refractive index of the material of the rings at the wavelength λ and the design temperature T_0 . Since each of the annular areas introduces a phase change of a $m_j 2\pi$ in the radiation beam at the design temperature, the phase structure does not change the wavefront of the radiation beam.

When the temperature changes, the stepped phase structure will change shape; 20 hence, the height of the rings will change. The refractive index of the material of the structure will also change. Consequently, the length of the optical paths through the annular areas will depend on the temperature of the phase structure. For a typical plastic material the coefficient of linear expansion α is approximately equal to $60 \cdot 10^{-6} / K$. The change β of the refractive index as a function of temperature, i.e. $\beta = dn/dT$, is typically equal to $-12 \cdot 10^{-5} / K$. The phase 25 change ϕ_j of ring j of the structure, the ring having a height h_j , is now determined for a temperature change of ΔT and relative to the phase of the structure at the temperature T_0 . If an isotropic expansion of the stepped structure is assumed, the phase change is given by

$$\phi_j = 2\pi \left[\frac{(h_j + \Delta h_j)(n + \Delta n - 1)}{\lambda} - m_j \right] = 2\pi \left[\frac{\Delta h_j}{h} + \frac{h_j \Delta n}{h(n-1)} \right] \quad (2)$$

where equation (1) has been used and terms quadratic in a difference have been neglected.

30 Since

$$\Delta h_j = \alpha h_j \Delta T = \alpha m_j h \Delta T$$

(3)

and

$$\Delta n = \beta \Delta T$$

(4)

5

the phase change is

$$\phi_j = 2\pi \left[\alpha + \frac{\beta}{n-1} \right] m_j \Delta T \quad (5)$$

Using the above parameter values, this gives

$$\phi_j = -0.00081 m_j \Delta T \quad (6)$$

10

If the optical head operates at a temperature of 50°C, i.e. $\Delta T = 30$ K, the objective lens introduces 36.1 mλ RMS temperature-induced spherical aberration. Figure 3 shows a cross-section of the wavefront W as a function of the normalised radius r of the radiation beam. The phase change ϕ_j introduced by ring j of height $m_j h$ at 50°C is now $-0.0243 m_j$ radians. The values of the integers m_j for each of the rings in the phase structure must be chosen such that

15 the phase structure will introduce a wavefront deviation that approximates the spherical aberration wavefront of Figure 3 but with opposite sign. Table I shows the results of the optimisation by the radii of the four annular areas shown in Figure 2, the height of each area and the relative phase of the radiation beam after passage through each area both for a temperature of 50°C and 0°C. In the latter case $\Delta T = -20$ K.

20

begin area (mm)	end area (mm)	height $m \cdot h$ (μm)	m	ϕ_j (50°C) (radians)	ϕ_j (0°C) (radians)
0.0	0.65	0	0	0	0
0.65	1.00	-13.464	-11	0.2673	-0.1782
1.00	1.53	-28.152	-23	0.5589	-0.3726
1.53	1.58	-11.016	-9	0.2187	-0.1458

Table I

A negative value of the height indicates a depression in the plate 50 instead of a rise as shown in Figure 2. Figure 4 shows the wavefront error at 50°C when both the objective lens and the compensator are arranged in the radiation beam. The wavefront error is now 12.6 mλ.

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Consequently, the compensator reduces the aberration of the objective lens caused by the

temperature change from a wavefront error of 36.1 mλ to 12.6 mλ. If the same phase structure is used at 0°C, the wavefront error is reduced from 16.9 mλ to 9.8 mλ RMS.

The compensator 16 and the objective system 18, shown as separate elements in Figure 1, may be integrated by arranging the phase structure 51 to 54 on a lens surface of the objective system. Preferably, the phase structure is arranged on an aspheric lens surface. If the aspheric surface is formed by a mould in a replication process, the phase structure can be incorporated in the mould. In this way the compensator can be added to the optical head at a very low additional cost.

In a second embodiment of the optical head the compensator 16 is used to compensate defocus caused by the collimator lens 14 when its temperature deviates from the design value. Since the distance between the radiation source 11 and the collimator lens 14 is fixed, the defocus will change the vergence of radiation beam 15 and, hence, the operation of the objective system 18. The compensator can be designed to introduce a temperature-dependent defocus in the radiation beam compensating the defocus of the collimator lens, following a procedure similar to the above procedure for compensating spherical aberration. The compensator may be integrated with the collimator lens into a single element.

The phase structures for the compensation of the spherical aberration and the defocus may be integrated in one compensator. This combined compensator may be integrated with the objective system or the collimator lens. The number of rings in the compensator is determined by a balance between several factors. A higher number of rings reduces the rest wavefront, such as shown in Figure 4, thereby improving the compensation. However, a higher number of rings decreases the manufacturability of the moulds. It also increases the number of steps in the phase structure, thereby increasing the loss of radiation energy by scattering on the imperfect edges of the steps.

Although the described embodiments of the compensator are used in transmission, it will be clear that the invention is also applicable to optical elements used in reflection.

24. 12. 1999

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CLAIMS:

1. An optical head for scanning an optical record carrier having an information layer, the head comprising a radiation source for generating a radiation beam, an optical system for converging the radiation beam to a focus on the information layer, the optical system imparting a temperature-dependent first wavefront deviation to the radiation beam, and
5 a compensator arranged in the radiation beam for compensating the first wavefront deviation, characterized in that the compensator comprises a phase structure of a material having temperature-dependent properties, the phase structure having the form of annular areas forming a non-periodic pattern of optical paths of different, temperature-dependent lengths, the optical paths forming a second wavefront deviation compensating the temperature-
10 dependent first wavefront deviation.
2. Optical head according to Claim 1, wherein the optical system comprises an objective system imparting spherical aberration as the first wavefront deviation to the radiation beam.
15
3. Optical head according to Claim 1, wherein the optical system comprises a collimator lens and an objective lens, the collimator lens being arranged closer to the radiation source than the objective lens, the objective lens imparting defocus as the first wavefront aberration to the radiation beam.
20
4. Optical head according to Claim 1, wherein the differences between the optical paths are multiples of the wavelength of the radiation beam for at least one temperature.
5. A device for scanning an optical record carrier having an information layer, the
25 device comprising an optical head according to Claim 1, 2, 3 or 4 and an information processing unit for error correction.
6. A set of optical elements comprising an optical element and a compensator, the optical element being arranged in the path of a radiation beam and imparting a temperature-

dependent first wavefront deviation to the radiation beam, the compensator being arranged in the path of the radiation beam for compensating the first wavefront deviation, characterized in that the compensator comprises a phase structure of a material having temperature-dependent properties, the phase structure having the form of annular areas forming a non-periodic pattern of optical paths of different, temperature-dependent lengths, the optical paths forming a second wavefront deviation compensating the temperature-dependent first wavefront deviation.

7. Set of optical elements according to Claim 6, wherein the differences between the optical paths are multiples of the wavelength of the radiation beam for at least one temperature.

8. Set of optical elements according to Claim 6 or 7, wherein the first wavefront deviation is spherical aberration.

9. Set of optical elements according to Claim 6 or 7, wherein the first wavefront deviation is defocus.

10. Set of optical elements according to any of Claims 6 to 9, wherein the optical element is a lens.

11. Set of optical elements according to Claim 6, wherein the optical element and the compensator are integrated in a single element.

ABSTRACT:

(90)

An optical head (1) for scanning optical record carriers (2) is provided with a compensator (16) for compensating spherical aberration of the objective system (18) or defocus of the collimator lens (14) caused by operation of the optical head at a temperature different from the design temperature. A surface of the compensator (16) comprises a phase structure in the form of annular areas (52, 53, 54), the areas forming a non-periodic pattern of optical paths of different length. The optical paths change as a function of temperature and form a temperature-dependent wavefront deviation that compensates the spherical aberration and/or defocus.

10 Figure 1

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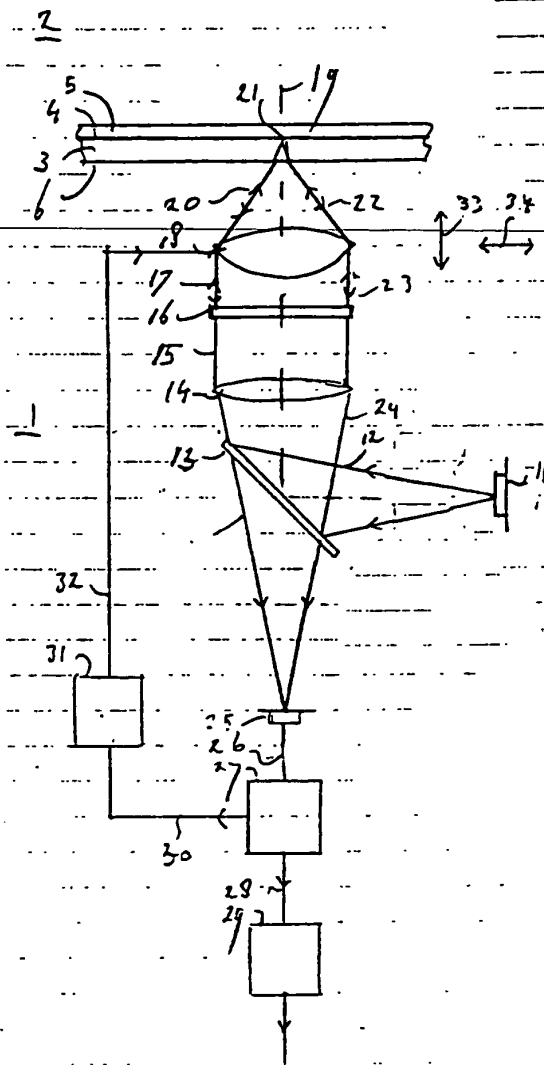


FIG. 1

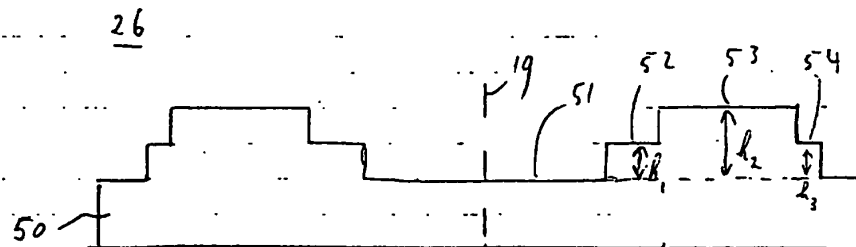


FIG. 2

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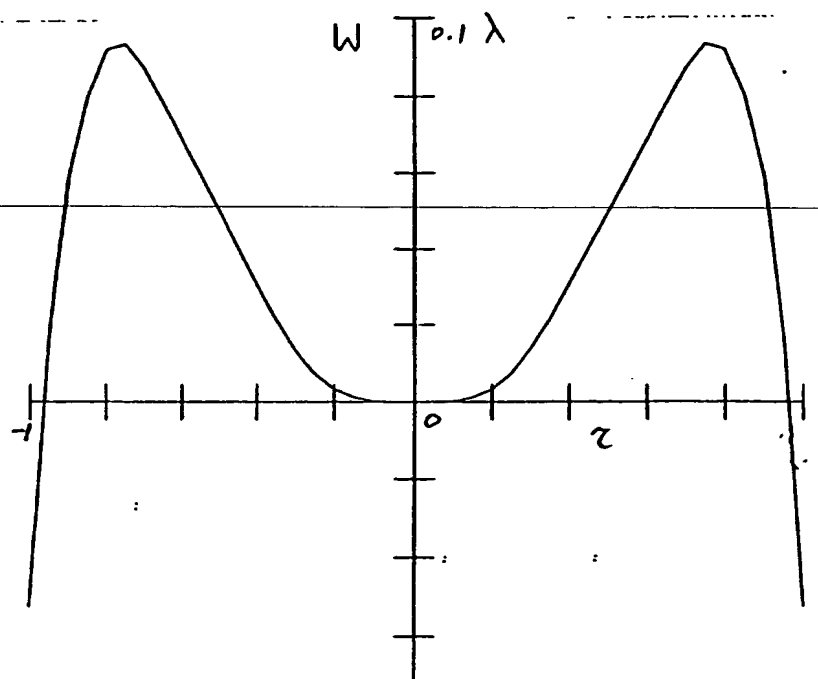


FIG. 3

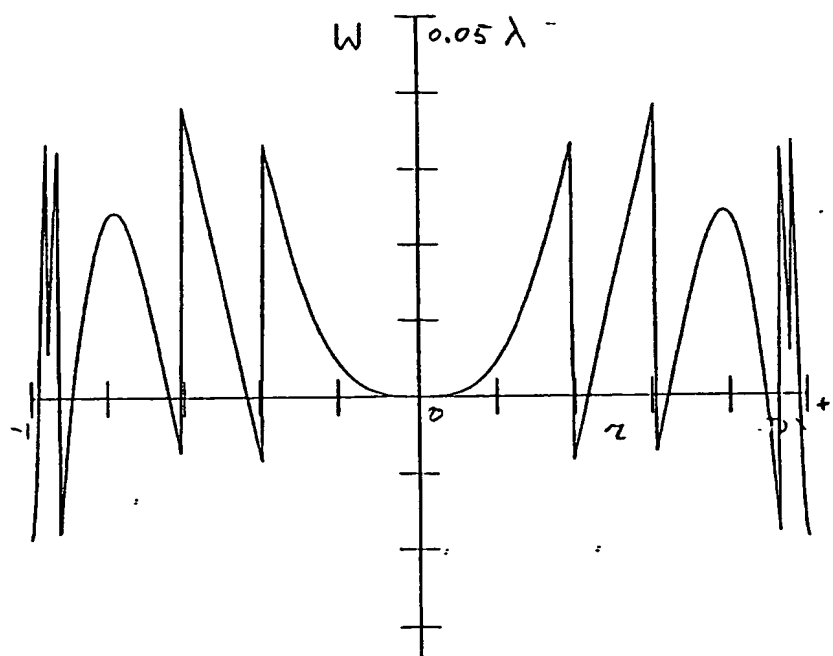


FIG. 4